

## VAPOR AND GAS TURBINES

### - EXERCISE n° 01 -

An impulse vapor turbine expands the fluid from the feeding conditions  $p_o = 100$  bar,  $T_o = 450$  °C, to the discharge conditions  $p_2 = 10$  bar,  $T_2 = 200$  °C, being negligible the kinetic energy change through the whole machine.

...Calculate the isentropic efficiency ( $\eta_{is,t}$ )

...Moreover, calculate the volume relative (or percent) change, which the vapor undergoes to, along the actual expansion process.

*Results:*

$$\eta_{is,t} \cong 0.762, PC(v) \cong 685.7 \%$$

### - EXERCISE n° 02 -

A vapor reaction turbine has the feeding conditions  $p_o = 120$  bar,  $T_o = 500$  °C and the isentropic efficiency  $\eta_{is,t} = 0.90$ . At the machine outlet, a saturated vapor mass flow rate is discharged.

...Find out the corresponding discharge pressure and temperature.

...Moreover, find the discharge "steam-to-liquid" ratio, which would be obtained if the expansion were isentropic.

*Results:*

$$p_{dsc} \cong 7.4 \text{ [bar]}, T_{dsc} \cong \dots \text{ [}^\circ\text{C]}, x \cong 0.955$$

### - EXERCISE n° 03 -

An axial turbine has the kinematic reaction index  $KDR = 0.5$ . The velocity triangles are symmetrical, with the angle  $\alpha_1 = 30^\circ$ , and show their configuration for maximum efficiency. The FDL coefficients are  $\varphi = 0.95$ ,  $\psi = 0.90$  and the kinetic energy change through the whole machine is quite negligible.

...Calculate the isentropic reaction index IDR (or  $\chi$ ).

*Results:*

$$IDR \cong 0.534$$

### - EXERCISE n° 04 -

A single stage vapor turbine (centripetal hybrid flow, with radial inlet and axial outlet) has the inlet diameter  $d_1 = 25$  cm and rotation speed  $n = 30'000$  rpm.

The feeding conditions are:  $p_o = 10$  bar,  $T_o = 380$  °C,  $S_o =$  entropy per unit mass. The discharge conditions are:  $p_2 = 3$  bar, while the entropy per unit mass ( $S_2$ ) is 2.5% lower than " $S_o$ ".

...Explain why the machine cannot be considered adiabatic and tell whether the fluid receives or loses heat.

...Draw a sketch of the velocity triangles with  $u_1 = 0.75 \cdot C_{u1}$ ,  $C_{u2} = 0$ ,  $C_2 = C_o$  (*distributor inlet*).

...Calculate the exchanged heat amount.

*Results:*

$$Q < 0, |Q| > L_w, Q \cong -192.383 \text{ [kJ/kg]}$$

## VAPOR AND GAS TURBINES

### - EXERCISE n° 05 -

Let's consider the following velocity triangles of a centripetal turbine:

At the runner inlet:  $C_{m1} = U_2$ ,  $C_{u1} = 4 \cdot U_2$

At the runner outlet:  $C_{m2} = 2 \cdot U_2$ ,  $C_{u2} = -U_2$

From inlet to outlet  $U_2 = U_1/3$ .

...Draw a sketch of the velocity triangles

...Calculate the kinematic reaction index (KDR) with  $C_{m1} = C_o$  (*distributor inlet*).

*Results:*

.KDR  $\cong$  0.538

### - EXERCISE n° 06 -

A Curtiss wheel with two bladed crowns on the runner disc shows the following design and working characteristics:

$\alpha_1 = 15^\circ$ ,  $C_{m1} = 100$  m/s,  $\sigma = U_1/C_1 = 0.2$ ,  $\varphi' = \varphi = 0.95$ ,  $\psi' = \psi = 0.90$ .

...Calculate the indicated work contribution of each individual bladed crown and the whole indicated work of the machine, according to the following cases:

A) symmetrical second distributor, with  $\alpha_3 = 180^\circ - \alpha_2$

B) asymmetrical second distributor, with  $\alpha_3 = \alpha_1$ .

*Results:*

. $L_{i,I} \cong 43.449$  [kJ/kg], A:  $L_{i,II} \cong 15.025$  [kJ/kg],  $L_{i,tot} \cong 58.474$  [kJ/kg],

. $L_{i,I} \cong 43.449$  [kJ/kg], B:  $L_{i,II} \cong 16.868$  [kJ/kg],  $L_{i,tot} \cong 60.314$  [kJ/kg]

### - EXERCISE n° 07 -

An adiabatic gas turbine expands air from the feeding conditions  $p_o = 7$  bar,  $T_o = 1300$  K to the discharge pressure  $p_s = p_a = 1$  bar (*atmospheric pressure*), with polytropic efficiency  $\eta_{yt} = 0.87$ , being negligible the kinetic energy change through the whole machine.

...Calculate the corresponding isentropic efficiency ( $\eta_{is,t}$ ) and discharge temperature ( $T_s$ )

...Moreover, calculate the following energy quantities per unit mass: the indicated work ( $L_{it}$ ), the isentropic work ( $L_{is,t}$ ), the FDL wasted work ( $L_w$ ), the equivalent energy head ( $g \cdot H_t$ ), the thermal recovery amount (RC).

*Results:*

. $\eta_{is,t} \cong 0.89921 \cong 0.899 \cong 0.90$ ,  $T_s \cong 801.449$  [K],  $L_{it} \cong 501.143$  [kJ/kg],  $L_{is,t} \cong 557.316$  [kJ/kg],

$L_{wt} \cong 74.883$  [kJ/kg],  $g \cdot H_t \cong 576.027$  [kJ/kg],  $RC \cong 18.711$  [kJ/kg].

## VAPOR AND GAS TURBINES

### - EXERCISE n° 08 -

A reaction gas turbine expands the fluid from the feeding conditions  $p_o = 9$  bar,  $T_o = 1400$  K to the discharge pressure  $p_s = p_a = 1$  bar (*atmospheric pressure*). Along the expansion a given heat amount is transferred to the gas in a gradual and continuous way, such to obtain a resulting constant-temperature process (*that is: "isothermic"*).

The FDL ( $L_{wt}$ ) are 13% of the equivalent energy head ( $g \cdot H_t$ ), while the kinetic energy change through the whole machine can be considered quite negligible.

... Calculate the heat supply per unit mass ( $Q$ ) and the corresponding indicated work per unit mass ( $L_{it}$ ).

Use:  $k' = 1.37$ ,  $R' = 292$  J/(kg·K)

*Results:*

$Q \cong 781.456$  [kJ/kg] ,  $L_{it} \cong 781.456$  [kJ/kg] , ( $Q = L_{it}$ ) .

\* \* \* \* \*